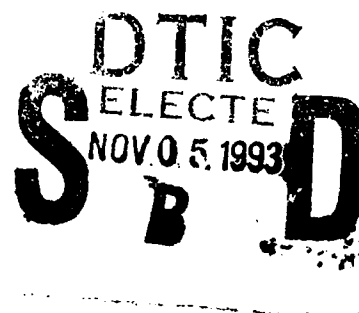




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NAVAL POSTGRADUATE SCHOOL Monterey, California



THESIS

DUAL-BEAM MULTIPLE-WAVELENGTH
LIGHT TRANSMITTANCE MEASUREMENT
FOR PARTICLE SIZING
IN ROCKET MOTOR PLUMES

by

Kevin B. Taylor

June, 1993

Thesis Advisor:

David W. Netzer

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Dual-Beam Multiple-Wavelength
Light Transmittance Measurement
for Particle Sizing in
Rocket Motor Plumes

by

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Submitted in partial fulfillment
of the requirements for the degree of

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ABSTRACT

A multiple-wavelength light transmittance measurement system previously used in a laboratory environment to study particles in solid rocket propellant exhaust plumes was modified for use in the field, where high levels of vibration can degrade the accuracy of data. The system was converted from a single light beam configuration to a dual beam configuration which was capable of obtaining a complete set of 1024 reference and scene measurements in 10 ms. Modifications included designing, building and testing a new analog-to-digital data converter trigger circuit, and a rotating-wheel light chopper. Optical components including beam splitters, lenses and a fiber optic cable were installed, and existing data collection system software was modified. The new system was tested by measuring soot from an oxy-acetylene torch to prove the design concept. Test results and system performance were documented. Recommendations for further-modifications, improvements and applications are presented.

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I. INTRODUCTION

During a recent war, a need for exhaust plume signature prediction and identification for liquid propellant rocket engines was realized. Since radiation emissions are greatly effected by particles in the plume, knowledge of their size, optical properties, and concentration provides valuable information which is needed to predict the exhaust signature. Liquid rocket propellants, unlike solid rocket propellants, do not normally contain any added metals which can enhance the signature of the plume. However, the exhaust can contain significant amounts of carbon particles, which result from the combustion of hydrocarbons. Soot can produce increased visible and infrared signatures.

Several methods for measuring particles in exhaust plumes exist. The most common procedures are particle sample withdrawal followed by optical measurements or in situ methods based on the transmission and/or scattering of light [Ref. 1]. Soot particles produced by liquid propellants are predominately in the submicron range [Ref. 2,3]. Measurement of these small particles can be accomplished using multiple-wavelength light transmission techniques [Ref 4].

Recent research at the Naval Postgraduate School by Vaughn [Ref. 1] and Kim [Ref. 5] successfully used multiple-

wavelength light transmission measurements for submicron aluminum oxide particles in the plumes of solid propellant rockets. This technique measured the transmittance at six wavelengths. The measured ln-transmittance ratios were compared to the extinction coefficient ratios obtained from a Mie-based computer code. The Beer-Lambert law for the exponential decay of light intensity through a uniform particle field could then be used to obtain the particle concentration [Ref. 4].

The apparatus used in these investigations, while accurate for small rocket motors in a controlled laboratory environment, would probably be greatly effected by vibrations caused by larger motors [Ref. 2]. The apparatus, as originally configured, collected all reference measurements for transmittance calculations prior to rocket motor ignition, which were then averaged to get a mean value. Light measurements through the plume were then collected after motor ignition, which were also averaged. Transmittance was obtained from the averaged values [Ref. 1,5].

Vibrations from a large motor firing can cause variations in the intensity of the light source and/or the alignment of the optical components, thus invalidating the averaged pre-run reference measurements [Ref. 2]. One way to overcome this limitation is to collect reference measurements simultaneously with plume measurements. Transmittance can then be calculated

at any instance of time, thus negating the effects of vibration and other variations during the burn time. These individual transmittances could then be averaged, if desired.

Another limitation of the light transmission and collection equipment was that it had only been tested across short distances (less than two feet) [Ref. 1,5]. Use of the apparatus on full scale rocket motors would require transmission lengths of fifteen feet or more.

The purposes of this investigation were to (1) modify the multiple-wavelength light transmission apparatus and associated data collection equipment used by Vaughn [Ref. 1] to obtain near-simultaneous reference and plume measurements, (2) extend the light transmission distance and (3) validate the modifications by measuring soot particles from a test source.

II. THEORETICAL BACKGROUND

A. INTRODUCTION

Multiple wavelength light transmission measurement techniques have been used extensively in recent years to study the nature of small particles. The theory behind these techniques is discussed in detail by Few [Ref. 2,6], Cashdollar [Ref. 4] and Vaughn [Ref. 1].

Recent particle sizing techniques using light transmission measurements are varied applications of the Mie theory for the light scattered by particles [Ref. 1,2]. For particles much smaller than the wavelengths of the incident light the Rayleigh approximation is often used. The techniques have been refined over the years, but the basic approach is that a collimated light beam is transmitted through a particle field [Ref. 2]. Particle size information is then provided by the wavelength dependence of the angular scattering and extinction of the light beam [Ref. 2].

The technique used in this experiment focused on using the extinction of light of multiple wavelengths to determine mean particle size and the particle index of refraction.

B. LIGHT TRANSMISSION/EXTINCTION THEORY

The transmission of light through a uniform particle cloud is given by the Beer-Lambert law [Ref. 4]:

$$T = \exp(-QAnL) = \exp\left(-\frac{3QC_p L}{2\rho d}\right) \quad (1)$$

where T = fraction of light transmitted,

Q = dimensionless extinction coefficient,

A = cross sectional area of a particle,

n = number concentration of particles,

L = path length,

C_p = mass concentration of particles,

ρ = density of an individual particle,

d = particle diameter

Mie scattering theory considers the interaction of a plane electromagnetic wave with a spherical object. Computation of Q as a function of particle size, light wavelength, and complex index of refraction is possible, and further extensions of the theory have been applied to nonspherical particles [Ref. 1,2,4].

This extension holds if the nonspherical particles are approximated by spherical particles whose diameters provide the same volumes as the nonspherical particles. [Ref. 1,2,6]

For a polydisperse system of particles, Dobbins [discussed Ref. 4] revised the transmission law to obtain:

$$T = \exp\left(-\frac{3\bar{Q}C_m L}{2\rho d_{32}}\right) \quad (2)$$

where \bar{Q} is the average extinction coefficient and d_{32} is the volume-to-surface mean (Sauter mean) particle diameter [Ref. 1,4].

Taking the natural logarithm of equation (2) yields:

$$\ln T = \bar{Q}\left(-\frac{3C_m L}{2\rho d_{32}}\right) \quad (3)$$

A multiple-wavelength light beam has identical L , ρ , C_m , and d_{32} for each wavelength through the plume. Therefore, the ratio of the \ln -transmissions at any two wavelengths is equal to the ratio of the calculated mean extinction coefficients for the same wavelengths [Ref. 1,4]:

$$\frac{\ln T(\lambda_i)}{\ln T(\lambda_j)}_{\text{experimental}} = \frac{\bar{Q}(\lambda_i, d_{32})}{\bar{Q}(\lambda_j, d_{32})}_{\text{theoretical}} \quad (4)$$

Cashdollar's computer code [discussed in Ref. 1,4], utilizing Mie theory, was used to generate the values of \bar{Q} .

Transmittances at the various wavelengths are determined experimentally. Previous transmittance measurements by Vaughn [Ref. 1] and Kim [Ref. 5] used a single light beam, as discussed in Chapter I. In a dual beam system, as used by Few [discussed in Ref. 2], a calibration measurement of the ratio of scene beam (S) intensity to reference beam intensity (R) is conducted prior to the introduction of soot particles, yielding [Ref. 2]:

$$R_{cal} = \frac{I_S(\lambda)}{I_R(\lambda)} \quad (5)$$

The same intensity ratio is then recorded with soot particles present in the scene beam. The transmittance of light at each wavelength is obtained as the ratio of the sample ratio to the calibration ratio [Ref. 2]:

$$T(\lambda) = \frac{R_{sample}(\lambda)}{R_{cal}(\lambda)} \quad (6)$$

The procedure for determining soot particle diameter requires calculation of Q for various assumed values of λ , d_{32} , $m=a-ib$ (complex index of refraction), and an assumed particle size distribution. If the assumed values are correct, calculated Q ratios will match the measured ln-transmission ratios for each of the wavelengths utilized. [Ref. 1,4]

Studies by Cashdollar [Ref. 4], Few [Ref. 2], and others [discussed in Ref. 2,4] report that the complex index of refraction of soot has a real part (a) value of 1.8 to 1.9. The complex part (b) has values ranging from 0.3 to 0.66. Additionally, the studies report that small particles in plumes often have a monomodal log-normal distribution. In this case the distribution is characterized by d_{32} and σ (standard deviation). [Ref. 1,4]

Since there are four unknown variables (d_{32} , σ , a, and b) a minimum of four independent ln-ratios are needed. Increased numbers of ln-transmission ratios increase the ability to find the best fit between experiment and theory. The values of d_{32} , σ , a, and b are found by finding the best fit-(in the least-squares sense) between the calculated and measured results. [Ref. 1,2]

III. EXPERIMENTAL APPARATUS

A. GENERAL ARRANGEMENT

Figure 1 shows the general arrangement of the light transmission and collection equipment. A variable beam splitter, directly in front of the light source, was used to split the light into scene (through-plume) and reference beams for transmittance measurements. The reference beam was redirected through a chopper and focused into a fiber optic cable, which was routed around the particle cloud. The scene beam passed directly through the chopper, a collimating lens, and then through the plume. The chopper provided alternating light measurements for the reference and scene beams. A second beam splitter was used to direct the reference beam from the fiber optic cable into the spectrograph.

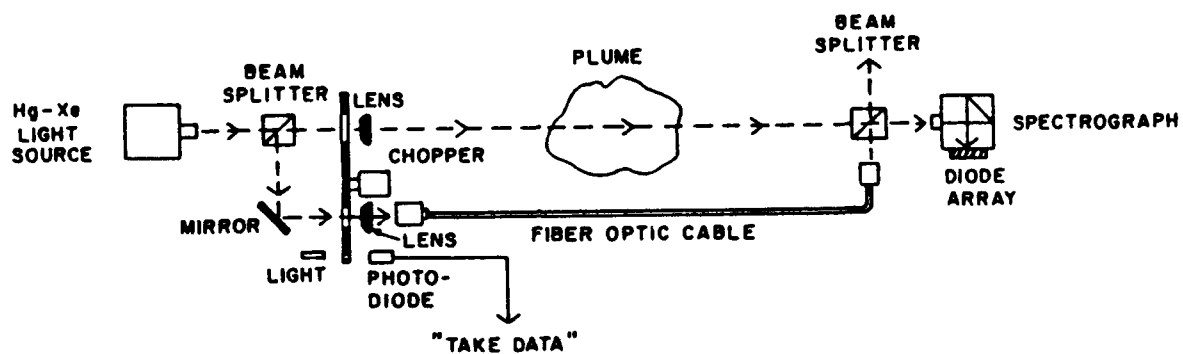


Figure 1
General Arrangement

A 200 Watt Mercury-Xenon bulb (Oriel Corp. #6291) was used as the light source in this experiment. It produced intensity peaks at wavelengths of 253.4, 302.2, 312.6, 334.2, 366.3, 404.7, 435.8, 546.1, and 577.0 nm. The bulb was mounted in a Oriel lamp housing with a F/1 condenser and a UV grade fused silica 1.5 inch lens. The lamp was powered by an Oriel power supply. [Ref. 7]

An Oriel model 77400 Multispec spectrograph was used to collect the reference beam and scene beam light intensities. A 25 μ m wide input slit restricted the the amount of stray light entering the spectrograph. The transmitted light was then projected onto a 1024 element diode array. Figure 2 shows the optical pattern within the spectrograph.

The diode array was an EG&G Reticon G series solid state line scanner with 1024 elements. Spectral response of the array is in the UV/IR range (approx. 200 - 1000 nm wavelength). The diode array was controlled by a Reticon RC100 motherboard which provided all clock, start, video amplifier, and blanking requirements. [Ref. 8]

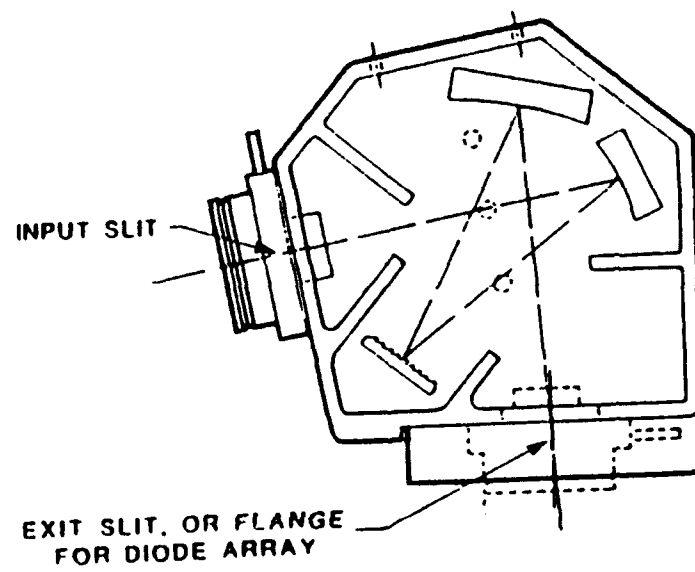


Figure 2
Multispec optical arrangement
[Ref. 7]

C. LIGHT CHOPPER

A detailed drawing of the light chopper disk is provided in Appendix A. The two sets of large apertures were designed to provide alternating reference and through-plume (scene) light measurements. The aperture arc length provided a transmission time of slightly more than the sweep time of the diode array (2.04 ms) when the disk was rotated at 1000 rpm. The small apertures on the outer radius provided a "take data" command signal to the Data Acquisition/Control System and were aligned with the leading edges of the large apertures. The light chopper provided 1024 transmittance values each 10.0 ms.

The chopper disk was driven by a Vexta model FBL-215A 24 volt DC speed control motor. The motor speed was controlled by a precision potentiometer. Speed was monitored by checking the frequency of the "take data" command from the chopper disk.

D. FIBER OPTICS

The reference beam was routed around the particle cloud using an Oriel, 600 μm diameter, UV/VIS single fiber optic cable. Cable length was 5 meters. Light was collected into the cable using an Oriel model 77780 Fiber Optic Input Accessory with a fused silica F/2 lens. Output from the cable was directed onto the second beam splitter using an Oriel model 77644 Collimating Beam Probe with fused silica lens.

E. OTHER OPTICS

Two types of beam splitters were used. The first type was a rotating disc, variable beam splitter which allowed for proportioning appropriate intensities of light into the scene and reference beams. A fused silica 50/50 polka-dot beam splitter was placed in front of the spectrograph. It was used to redirect the reference beam into the spectrograph entrance slit.

IV. DATA ACQUISITION SYSTEM

A. OVERVIEW

Data and clock/timing signals from the diode array were sent to a Hewlett Packard 6942A Multiprogrammer where the data were converted from analog to digital and stored on memory cards for processing. The multiprogrammer was programmed by a HP 9836S desktop computer. Figure 3 is a block diagram showing the general arrangement of the data acquisition system.

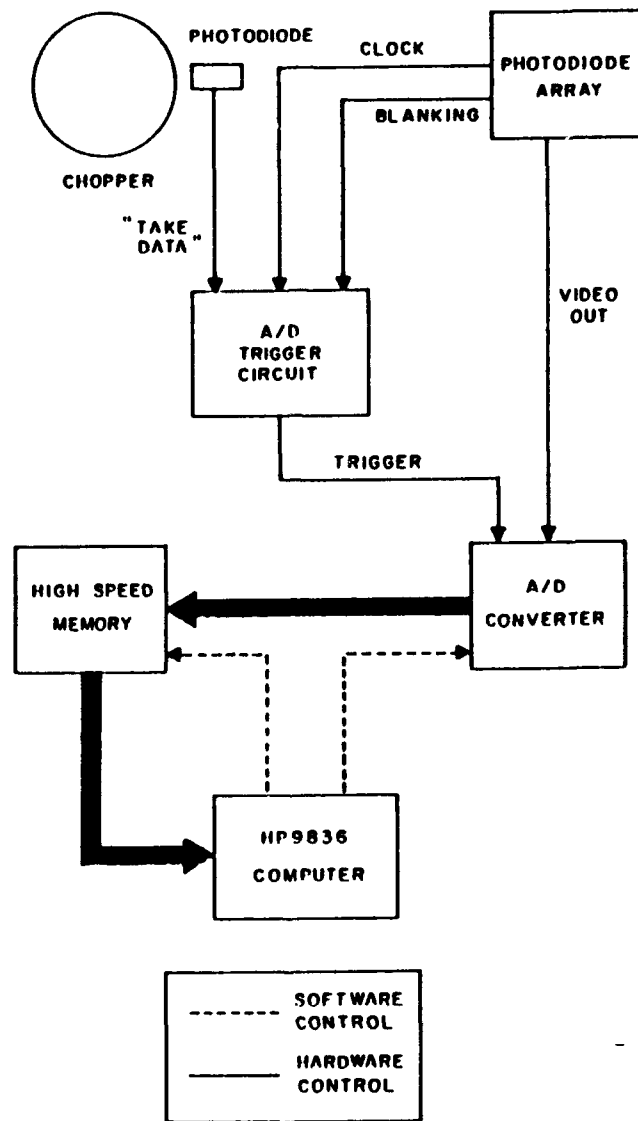


Figure 3
 Data Acquisition System
 [Adapted from Ref. 9:p. 40]

B. MULTIPROGRAMMER

The HP6942A Multiprogrammer is a self-contained system which has a wide variety of data acquisition applications. The system can accomodate up to sixteen I/O cards which are programmable by a desktop computer through the HP Interface bus. The cards can be addressed and controlled by the computer via the Multiprogrammer backplane or can be controlled by external triggers through rear card edge connectors. [Ref. 10:pp. 1-1, 2-1, 3-1, Ref. 1: p. 39]

The system used in this experiment was configured with one HP69759A 500 KHz A/D Converter card, one HP69791A High Speed Memory card and four HP69792A Memory Expansion cards.

1. 500 KHz A/D Card

The 500 KHz A/D card, when triggered, converts input voltages into 12-bit, twos-complement binary values within 2.0 μ s. It may be triggered internally by program command or externally by a lockout input at the edge connector. Digital output is available at the edge connector at a rate of 500 KHz. [Ref. 11]

The system was configured to receive analog data from the diode array and send digital data to memory at the edge connector. Additionally, it was configured for external triggering from the A/D trigger circuit.

2. High Speed Memory and Memory Expansion Cards

The High Speed Memory card can store up to 65,536 16-bit words at high speed. Data can be written to, or read from, the card by the computer via the backplane or an external device via the card edge connector. Memory Expansion cards are added to the Memory card by a special chaining cable. Each expansion card can store up to 196,608 16-bit words. With four expansion cards, the total memory available was 851,968 16-bit words. [Ref. 12]

Memory was programmed to operate in a First In/First Out (FIFO) mode. This allowed the cards to act like a data buffer with data written to sequential memory locations. [Ref. 12]

Data from the A/D card was written to memory via the edge connector. Data was then read from memory to the computer hard disk by the computer via the Multiprogrammer backplane.

C. A/D TRIGGER CIRCUIT

1. Purpose

The most critical part of the Data Acquisition System was the A/D trigger circuit. The circuit design had to insure that the Diode Array Clock signal (500.0 KHz), the Diode Array Blanking Pulse signal (484.5 Hz), and the "Take Data" command (200.0 Hz) from the chopper were properly combined. The resultant trigger signal was required to be a group of 1024 pulses (at 500 KHz) which were synchronized with the start of a diode array sweep and the leading edge of a chopper disc aperture. Figure 4 is a diagram showing how the signals were combined.

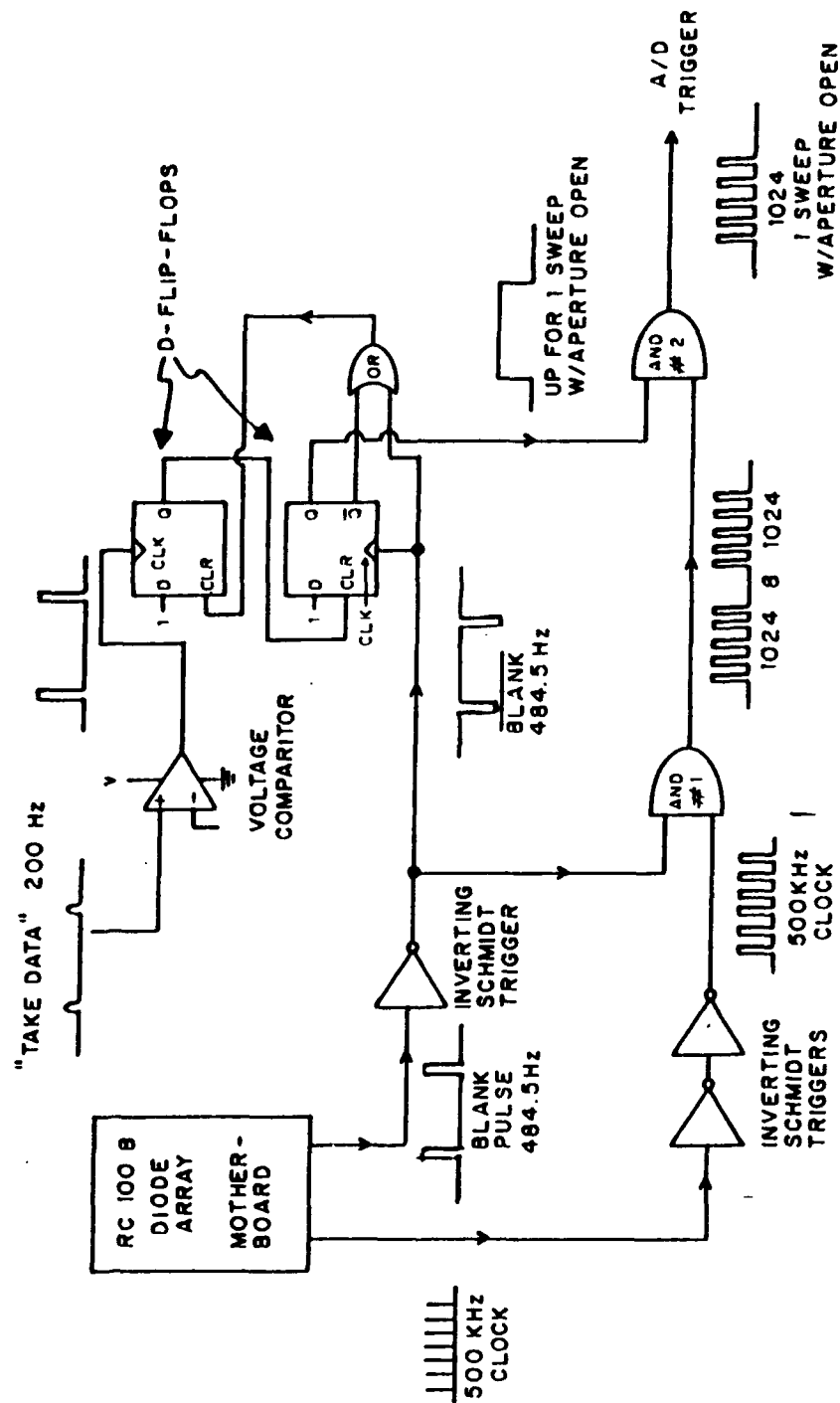


Figure 4
A/D Trigger Circuit

2. Modifications

During previous applications a Timer/Pacer card was programmed as an input to the A/D trigger signal, and a circuit card for the trigger was constructed [Ref. 1:p. 41, Ref. 9:p. 42]. Since the Timer/Pacer portion was deleted and the chopper "Take Data" signal (an analog voltage signal from a photodiode) was added, a new circuit card had to be designed and constructed, as previously discussed.

The new circuit card was installed and successfully tested. Figure 5 is a timing diagram of the A/D trigger circuit. A detailed drawing of the new circuit card is provided in Appendix B.

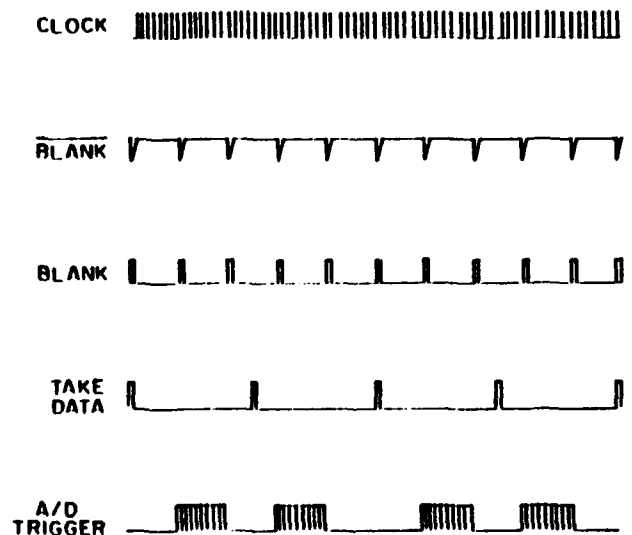


Figure 5
A/D Trigger Timing Diagram

V. SYSTEM TEST PROCEDURE AND RESULTS

A. TEST PROCEDURE

1. Initial Alignment

The system was initially constructed with the light source and spectrograph at a 10.0 ft. separation. The optics were then aligned and diode array voltages checked for both the reference and scene beams. The variable beam splitter was adjusted to provide optimum light intensities for both beams.

It became readily apparent that the 200 watt light source provided insufficient radiant power to overcome both being passed through two beam splitters and the losses in the fiber optic cable. With the best beam splitter adjustment and system optical alignment diode array peak voltages were barely discernable above base noise levels. The data acquisition system was unable to record usable readings for transmittance calculations.

2. Test Configuration and Procedure

Due to time and cost constraints, it was not possible to obtain a more powerful light source. The system was reconfigured so that sufficient diode array voltages were obtained to prove design concept. The variable beam splitter was removed and light was directed through the chopper into the fiber optic cable. The beam splitter at the entrance to

the spectrograph was removed and the output of the fiber optic cable was directed into the spectrograph. Reference beam intensities were obtained and averaged. It was then assumed that reference beam intensities were constant for the remainder of the system test.

The system was then configured to obtain test data from a particle source. The fiber optic cable was removed and the scene beam was directed through the chopper and directed onto the spectrograph inlet slit. Additionally, the spectrograph was moved to distance of approximately 4.0 ft. from the light source in order to insure sufficient scene beam intensity. Calibration (no plume) intensities were recorded prior to the introduction of soot particles. The smoke cloud from a fuel-rich oxy-acetylene torch flame was directed into the scene beam and intensities were recorded.

B. TEST RESULTS

1. Data Reduction

The first step in data reduction was to obtain calculated extinction coefficient (Q) ratios using the Mie-scattering computer code. Q was determined as a function of d_{32} , σ , m , and wavelength. Five wavelengths were observed during the test ($\lambda_1 = 366.3$, $\lambda_2 = 404.7$, $\lambda_3 = 435.8$, $\lambda_4 = 546.1$, and $\lambda_5 = 577.0$ nm) which provided ten independent ln-transmittance ratios.

Three values of m were used in the calculations. The first, $m = 1.8 - 0.3i$, is similar to the value derived by Kunitomo and Sato for various soots and the value measured by Chippett and Gray for propane and acetylene soots. The second, $m = 1.95 - 0.66i$, is the complex index of refraction of carbon measured by Senftleben and Benedict. The third, $m = 1.8 - 0.6i$, is an average of the index for carbon and the index for propane and acetylene soots measured by Dalzell and Sarofim. Two values of σ were used, 1.5 and 2.0, which are typical of soot particle size distributions. [Ref. 4]

The measured intensities were then converted into \ln -transmittance ratios. The average of six sweeps of the diode array were used to determine the reference beam intensities for five observed wavelengths. The intensities for the scene beam, both with and without particles, were similarly calculated using the averages from two sweeps of the diode array. The transmittances for each wavelength were then calculated as discussed in Chapter II. The natural logarithms were computed and the ten independent \ln -transmittance ratios (for five wavelengths) were obtained.

The next step in data reduction was to look for rough trends in data to reduce the amount of required regression analysis. Values for d_{32} were calculated using the measured \ln -transmittance ratios and various specified values of m and σ as shown in Table 1. The refractive index

$m = 1.8 - 0.6i$ with $\sigma = 1.5$ or 2.0 provided a poor correlation since six of the ten measured \ln -transmittance ratios were lower than the minimum calculated extinction coefficient ratios. Additionally, $m = 1.95 - 0.66i$ with $\sigma = 2.0$ yielded poor results. These three data sets were eliminated from further consideration. Calculations of mean d_{32} indicated a likely value ranging from approximately 0.10 to 0.17 microns.

TABLE 1
Calculated d_{32} for Specified m and σ Values

ln - ratios	m = 1.8 - 0.3		m = 1.95 - 0.66		m = 1.8 - 0.6	
	sigma = 1.5	sigma = 2.0	sigma = 1.5	sigma = 2.0	sigma = 1.5	sigma = 2.0
0.4884	0.14	0.06	0.06	**	**	**
0.5865	0.15	0.09	0.1	**	**	**
0.6106	0.18	0.125	0.125	0.085	0.12	0.065
0.6296	0.14	0.07	0.09	**	**	**
0.7332	0.21	0.17	0.155	0.12	0.15	0.115
0.7758	0.135	0.08	0.09	**	**	**
0.7872	0.22	0.2	0.155	0.12	0.16	0.115
0.7999	**	**	**	**	**	**
0.8328	0.09	0.06	0.06	**	**	**
0.9135	0.2	0.12	0.12	0.08	0.12	0.065
mean diam.	0.163	0.108	0.106	0.101	0.138	0.09
std dev.	0.04	0.047	0.036	0.019	0.018	0.025

Note: all values of d_{32} are in microns

** indicates ln-transmittance ratio below
minimum extinction coefficient ratio

Now that a likely range of values for d_{32} was obtained, the ratios of calculated mean extinction coefficients for assumed values of m , σ , and d_{32} were plotted against observed values of the \ln -transmittance ratios. If the ratios had corresponded exactly with each other, the data points would have formed a 45 degree line passing through the origin. Short of this, the best fit of data would have the least scatter about this line, and would form a line with a slope approximately equal to one. [Ref. 1]

The best fit of data was found by applying a linear least-squares fit to the data. The regression analysis function in Microsoft Excel was ideal for this purpose. The correlation coefficient, r , is a measure of the relationship between the \ln -transmittance ratios and the extinction coefficient ratios. The square of the correlation coefficient expressed as a percentage was used to measure how closely the data points matched the regression line. The r^2 values closest to one indicated the best linear correlation between data. The x - coefficient (slope) of the regression analysis indicated how closely the slope of the least-squares fit matched a 45 degree line. [Refs. 1, 13]

Figures 6, 7 and 8 are plots of the regression lines for $m = 1.8 - 0.3i$ ($\sigma = 1.5$), $m = 1.8 - 0.3i$ ($\sigma = 2.0$), and $m = 1.95 - 0.66i$ ($\sigma = 1.5$), respectively. Particle diameter (d_{32}) was varied from 0.09μ to 0.18μ in each case.

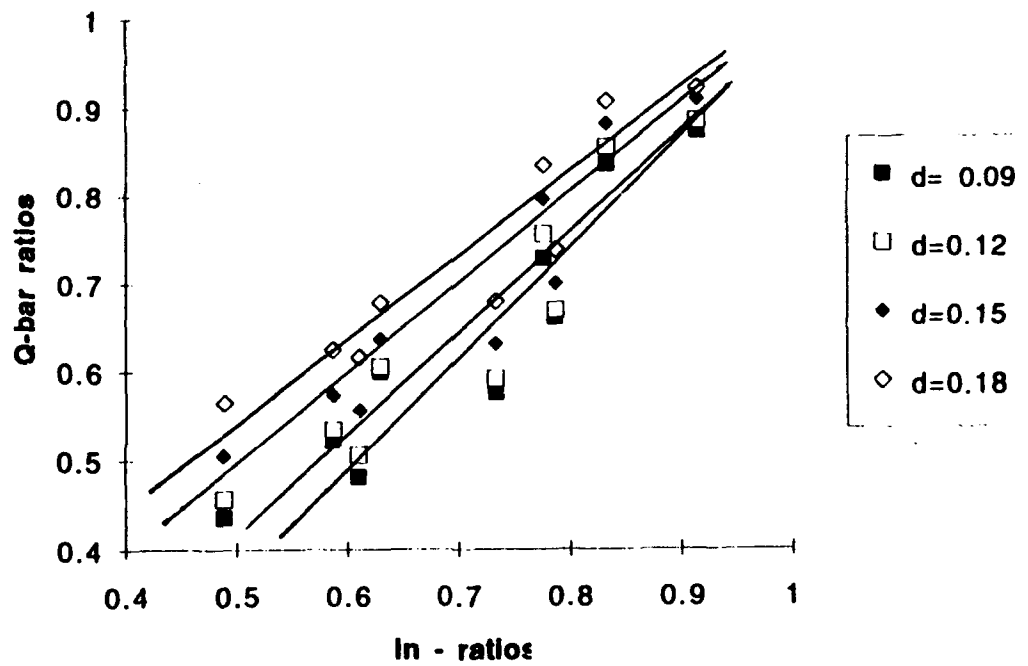


Figure 6
Least Squares Fit
 $m = 1.8 - 0.3i$ ($\sigma = 1.5$)

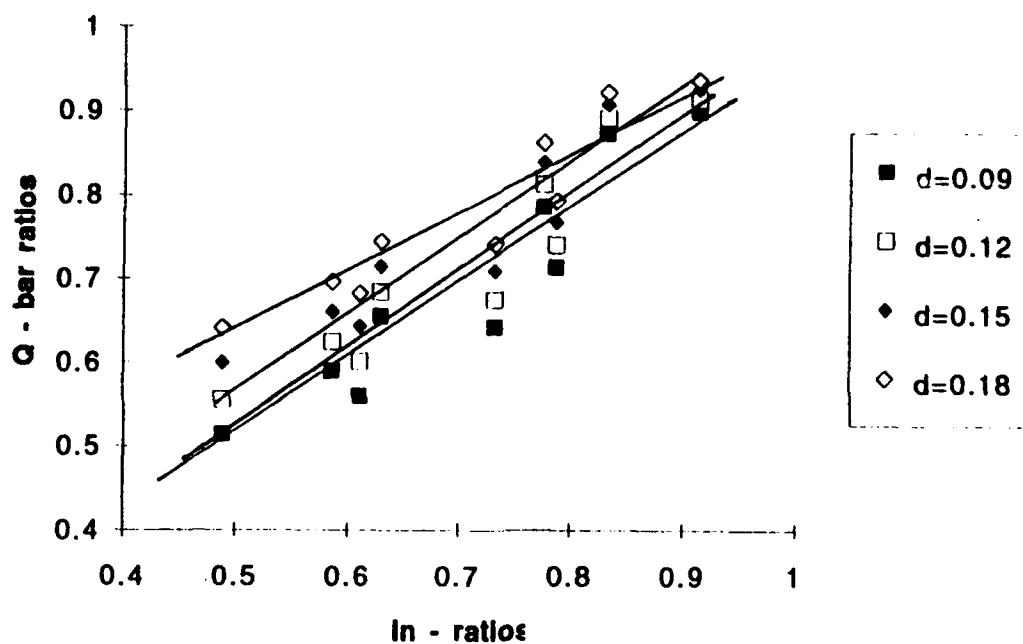


Figure 7
Least Squares Fit
 $m = 1.8 - 0.3i$ ($\sigma = 2.0$)

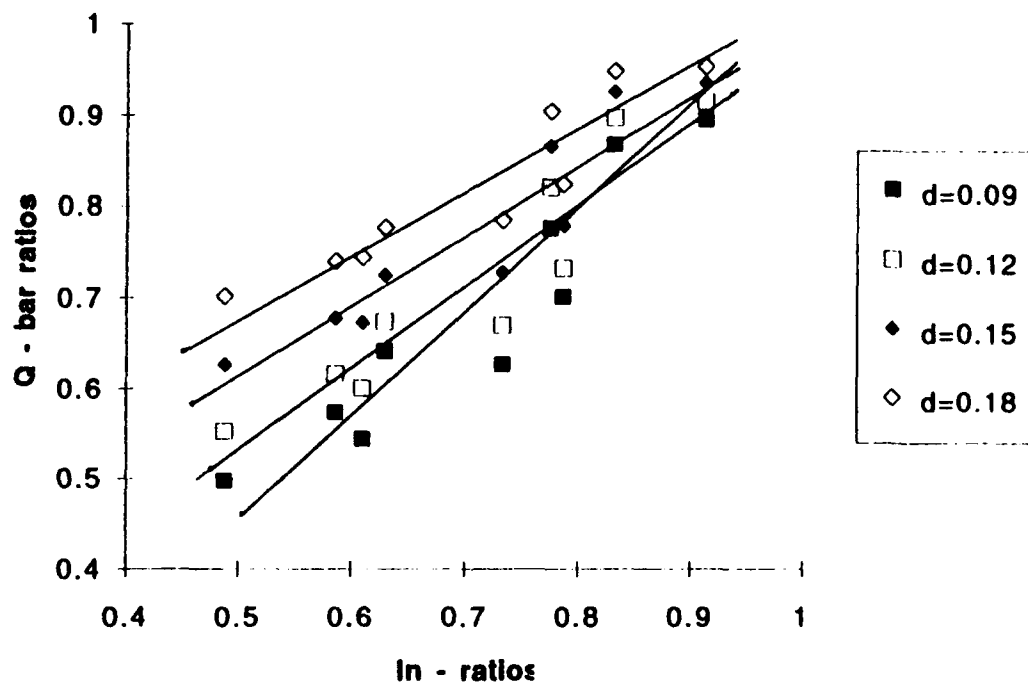


Figure 8
Least Squares Fit
 $m = 1.95 - .66i$ ($\sigma = 1.5$)

2. Data Analysis

As previously noted, Table 1 data indicated that $m = 1.8 - 0.6i$ with $\sigma = 1.5$ or 2.0 and $m = 1.95 - 0.66i$ with $\sigma = 2.0$ provided poor correlation. No correlations were obtainable using a ratio of $\ln T(\lambda_s=577.0\mu)$ over $\ln T(\lambda_s=546.1\mu)$. This apparently resulted because the wavelengths were so closely spaced [Ref. 5].

Table 2 lists the r^2 and x -coefficient values obtained in each case. The best r^2 value was 0.8839 for $d_{32} = 0.12\mu$, $m = 1.8 - 0.3i$, and $\sigma = 2.0$. All other r^2 values were within 2.0 percent. The best x - coefficient value was 0.995 for $d_{32} = 0.15\mu$, $m = 1.8 - 0.3i$, and $\sigma = 1.5$. This was significantly closer to 1.0 than any of the other results, indicating that d_{32} is probably closer to 0.15μ than 0.12μ . The poor correlations indicate the possible existence of a bimodal particle distribution in which the second mode is at a larger diameter as a result of soot agglomeration in the fuel-rich post-flame region, where the measurements were made.

It must be noted that the system recorded many more sweeps of the diode array than were actually used. Better results will be obtained by using all available data to calculate measured transmittances.

TABLE 2

Summary of r^2 and x - coefficient Values

diameter	m = 1.8 - 0.3 sigma = 1.5		m = 1.8 - 0.3 sigma = 2.0		m=1.95-0.66 sigma = 1.5	
	r - squared	x - coefficient	r - squared	x - coefficient	r - squared	x - coefficient
0.09	0.8809	1.0538	0.8837	0.9406	0.8806	0.9715
0.12	0.8759	1.0486	0.8839	0.8789	0.8753	0.8999
0.15	0.8739	0.995	0.8838	0.8057	0.8705	0.7783
0.18	0.8699	0.8919	0.8834	0.7317	0.8643	0.6408

3. System Performance

With the exception of an inadequate light source, system performance appeared to be excellent. The A/D trigger circuit and light chopper functioned as designed. One shortcoming in system software was noted. If the data acquisition program was actuated during an A/D trigger pulse group, then the recorded data was obtained out of sequence. This problem was mitigated by slowing the chopper rotation frequency, and thus the frequency of the "take data" signal. This resulted in longer nulls between A/D trigger pulse groups and, therefore, less chance of actuating the data acquisition program during a trigger group. The slower chopper rotation rate, and resulting slower data acquisition rate, could result in degraded performance in a high vibration environment.

VI. CONCLUSIONS AND RECOMMENDATIONS

A. CONCLUSIONS

The system design concept was proven valid. The goals of obtaining rapid measurements of reference and scene beam intensities and of extending the distance between light source and spectrograph were not achieved. Installation of a stronger light source will make these goals possible. Poor correlation of the data obtained from a fuel-rich oxy-acetylene flame was probably the result of the existence of a multimodal particle size distribution.

B. RECOMMENDATIONS

Recommendations for further system development and applications are:

(1) Obtain a more powerful light source. Minimum power should be 1000 watts.

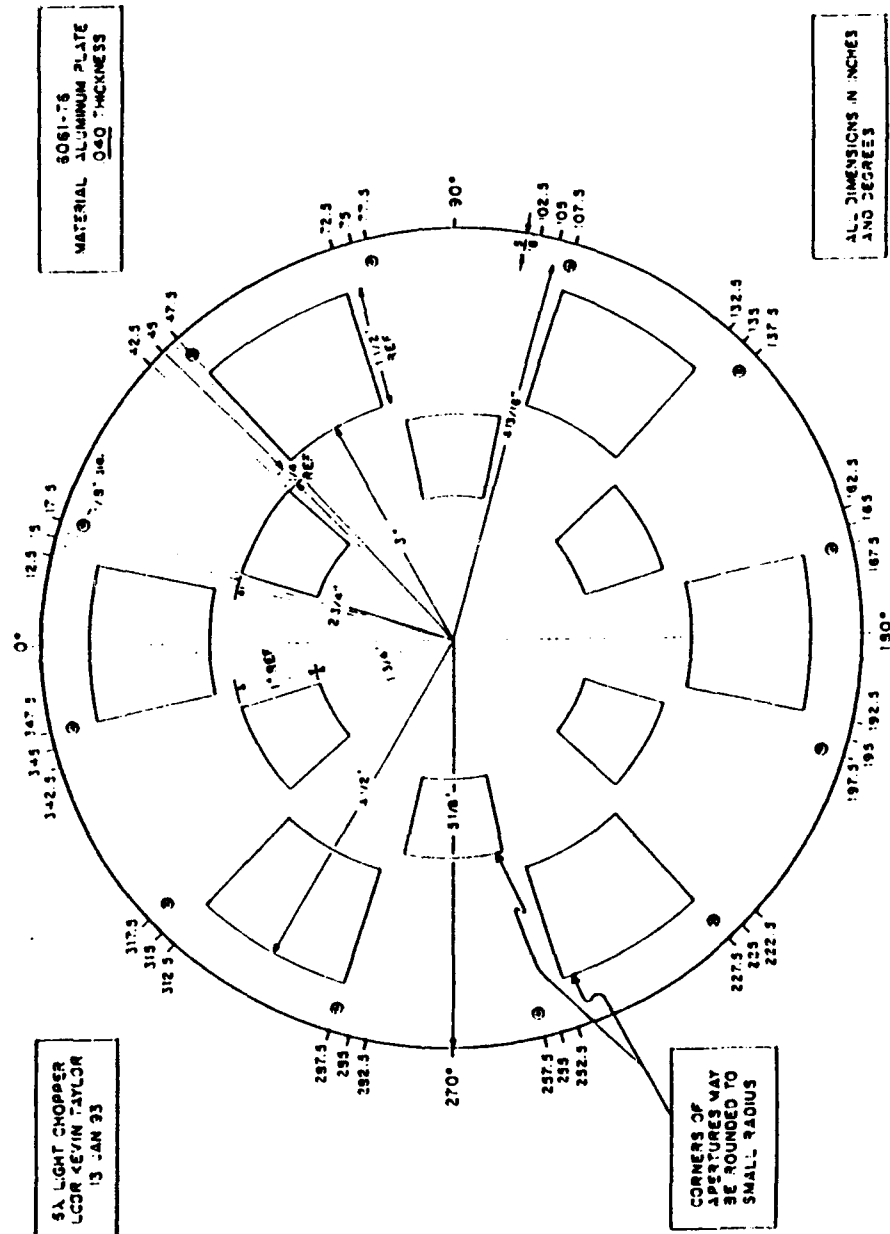
(2) When adequate intensities are obtained in both the scene and reference beams, test the system on a particle source with known characteristics.

(3) Conduct tests in environments with varying amplitudes and frequencies of vibration to determine system limitations.

(4) If the system is sensitive to vibrations with amplitudes and frequencies expected in the field environment, it may be necessary to reduce the number of diodes swept (since only approximately 10 of the 1024 are needed). This will result in a increased sweep rate (since $T_{\text{sweep}} = \# \text{ diodes in array} / 500 \text{ KHz}$). Additionally, a chopper capable of rotating at higher speeds will provide a higher data acquisition rate, since a higher "take data" signal frequency would result. The data acquisition program and/or the A/D trigger circuit would require modifications to eliminate the problem of triggering the A/D card in the middle of a trigger pulse group.

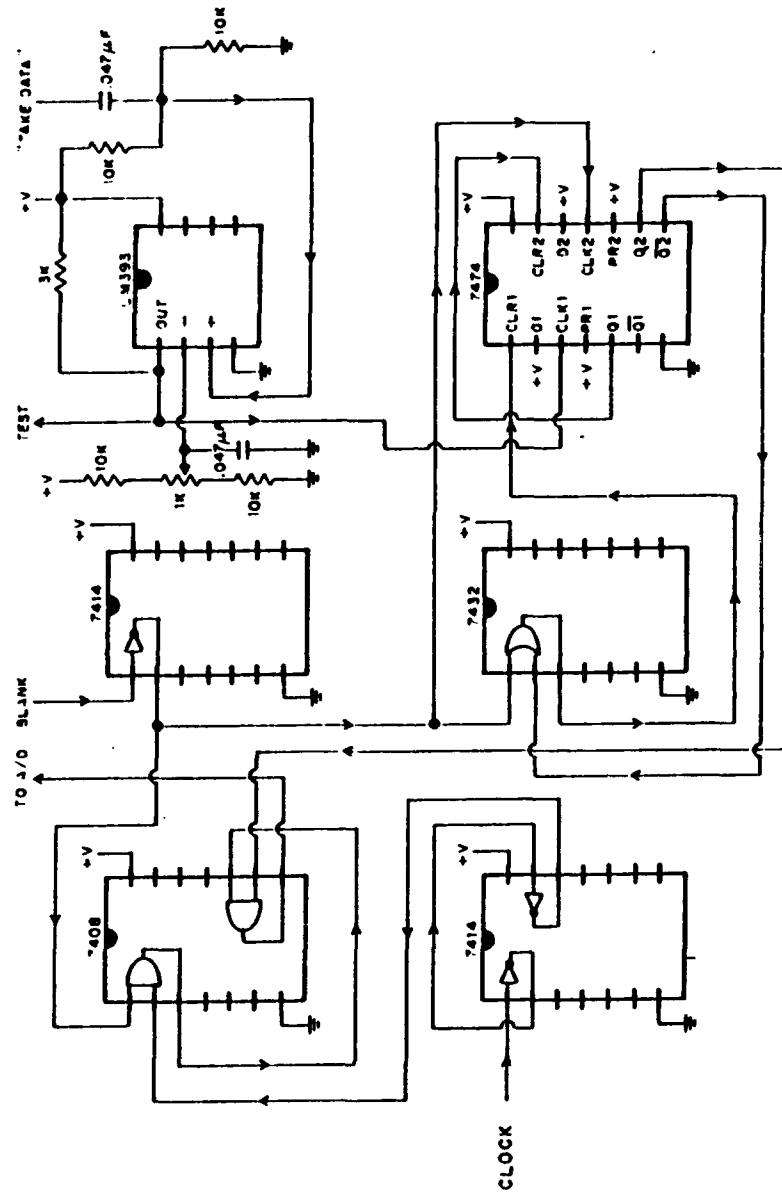
(5) Obtain the fiber optic cable and lenses required to extend transmission distance to that required for testing over longer distances (~40 ft).

APPENDIX A **LIGHT CHOPPER DISC DESIGN**



APPENDIX B

A/D TRIGGER CIRCUIT CARD SCHEMATIC



APPENDIX C

DATA ACQUISITION PROGRAM

```

20  !***** ACQUIRES MULTIPLE SCANS OF DIODE ARRAY *****
30  !***** AND STORES THEM ON DISK *****
40  !***** BERT HANSEN, KEN GRAHAM, KELLY HARRIS 1984 *****
41  !*****
50  !***** REVISED FOR USE WITH 500KHZ A/D AND STORAGE *****
51  !***** ON HARD DRIVE BY JIMMY VAUGHN 1992 *****
61  !***** REVISED FOR DUAL BEAM APPLICATION *****
70  !***** BY KEVIN TAYLOR 1993 *****
71  DIM C(1:8192),D(1:8192),Z(1:8192)
120 LOCAL LOCKOUT 7 ! DISABLES FRONT PANELS OF DATA ACQUISITION SYSTEM
130 REMOTE 709
140 OUTPUT 709;"AR" ! ANALOG RESET OPENS ALL CHANNELS
270 GOSUB Initiate
410 PRINT USING "0"
420 PRINT " DATA WILL BE STORED ON HARD DRIVE WITH FOLLOWING FILE NAMES:"
430 PRINT USING "///"
440 PRINT " CALIBRATION ---- A "
450 PRINT " PARTICLE SAMPLE ---- B "
452 OUTPUT 709;"DC11,2" ! OPEN SHUTTER
460 PRINT USING "///"
743 PRINT "TAKING DATA"
744 !WAIT 3
754 GOSUB Multiprog !Takes calibration data
755 GOSUB Perge
761 GOSUB Storedata
780 PRINT USING "/////////"
990 PRINT " INTRODUCE PARTICLES THEN PRESS KEY # 9 TO TAKE DATA"
1000 ON KEY 9 LABEL " TAKE DATA" GOTO 1011
1010 Standby:GOTO Standby
1011 Part=1
1012 PRINT USING "///"
1014 PRINT "TAKING PARTICLE DATA"
1015 WAIT .1
1020 GOSUB Multiprog
1040 ! TAKE PARTICLE DATA
!PARTICLE DATA FILE NAME
1057 GOSUB Storedata
1081 OUTPUT 709;"AR"
1082 LOCAL 7
1090 GOTO 3000
1100 Multiprog:
1101 Cdelay=0
1103 OUTPUT 709;"DC11,2"
1117 Cdelay=Cdelay+1
1127 IF Cdelay<5 THEN
1137 GOSUB Initiate
1147 GOTO 1117
1157 END IF
1305 IF Part=0 THEN
1309 PRINT USING "///"
1311 PRINT "CALIBRATION DATA IS STORED ON MEMORY CARDS "
1312 WAIT 3
1314 END IF
1320 IF Part=0 THEN GOTO 1590
1330 PRINT USING "///"
1404 PRINT "PARTICLE DATA IS STORED ON MEMORY CARDS "
1590 RETURN

```

A/D is in slot 1
 Mem Card 2,3
 Timer/pacer 8
 Mem Exp Cards 4,5,6,7

```

1600 Storedata:1
1601 PRINT USING "///"
1602 PRINT "DATA IS BEING TRANSFERED FROM THE CARDS TO THE COMPUTER"
1603 PRINT USING "/"
1605 PRINT "WHEN THE TRANSFER IS COMPLETE THE FIRST 5 ENTRIES OF EACH FILE"
1606 PRINT "          WILL BE DISPLAYED"
1607 OUTPUT 723;"WF2.3,76T"          !FIFO-IN WITH LOCKOUT
1608 OUTPUT 723;"MI";2;8192;"T"
1609 ENTER 72305;Z(*)
1612 IF Part=1 THEN GOTO 1700
1613 PRINT "NEGATIVE VOLTAGE LOOP"
1615 FOR I=1 TO 8192
1616 IF Z(I)<32000 THEN
1617 C(I)=Z(I)*.0005
1618 GOTO 1630
1619 END IF
1621 C(I)=(65535-Z(I))*0.0005
1630 NEXT I
1650 GOTO 1702
1700 Part=Part+1
1701 PRINT "NEGATIVE VOLTAGE LOOP"
1710 IF Part=1 THEN GOTO 1607
1720 FOR I=1 TO 8192
1730 IF Z(I)<32000 THEN
1740 D(I)=Z(I)*.0005
1741 GOTO 1751
1742 END IF
1750 D(I)=(65535-Z(I))*0.0005
1751 NEXT I
1760 Part=1
1775 PRINT USING "///"
1782 Lucky$=CHR$(65)
1783 ASSIGN @Path2 TO Lucky$
1784 OUTPUT @Path2;C(*)
1785 IF Part=0 THEN GOTO 1790
1787 Lucky$=CHR$(64)
1788 ASSIGN @Path2 TO Lucky$
1789 OUTPUT @Path2;D(*)
1790 FOR I=65 TO 65:Part
1791   Lucky$=CHR$(I)
1792   ASSIGN @Path2 TO Lucky$
1793   PRINT "DATA ";CHR$(I)
1794   FOR J=1 TO 5
1795     ENTER @Path2;N
1796     PRINT N
1797   NEXT J
1798 NEXT I
1799 WAIT 3
1801 OUTPUT 723;"WF2.3,56T"          !FIFO-IN WITHOUT LOCKOUT
1802 RETURN

```

```

1840 Initiate:
1880 OUTPUT 723;"WF,2.3,256,2.3,56,T"!Initialize the Mode register
1881 OUTPUT 723;"WF,2.1,30,2.2,0,T"!Set reference 2(low order word)
1882 OUTPUT 723;"WF,2.1,31,2.2,0,T"!Set reference 2(high order word)
1883 OUTPUT 723;"WF,2.1,26,2.2,17777,T"!Set reference 1(low order word)
1884 OUTPUT 723;"WF,2.1,27,2.2,17,T"!Set reference 1(high order word)
1885 OUTPUT 723;"WF,2.1,22,2.2,0,T"!Reset Read Pointer(low order word)
1886 OUTPUT 723;"WF,2.1,23,2.2,0,T"!Reset Read Pointer(high order word)
1887 OUTPUT 723;"WF,2.1,20,2.2,0,T"!Reset the Difference counter(low order word)
1888 INPUT 723;"WF,2.1,21,2.2,0,T"!Reset the Difference counter(high order
word)
1889 OUTPUT 723;"WF,2.1,24,2.2,0,T"!Reset the Write pointer(low order word)
1890 INPUT 723;"WF,2.1,25,2.2,0,T"!Reset the Write pointer(high order word)
1891 OUTPUT 723;"CC,2,1"!Send a clear card instruction
1892 PRINT USING "3/"
1893 OUTPUT 723;"WF,2.3,56T"      !SET MEMORY CARD TO FIFO-IN MODE
1894 OUTPUT 723;"CY",2,"T"      !ACTIVATE CARD
1895 OUTPUT 723;"WF1.1,11,1.2,0T" !DISABLE MUX(Need to enable mux if ever
!switch back to 1417A connector cable)
1896 OUTPUT 723;"WF1.1,12,1.2,0T" !DSBL OUTPUT FALSE
1897 OUTPUT 723;"WF1.1,13,1.2,0T" !ENBL EFN FALSE
1898 OUTPUT 723;"WF1.3,0T"      !RESET A/B MODE BITS
1899 OUTPUT 723;"WF1.1,2,1.2,1T" !SET EXTERNAL TRIGGER
1900 OUTPUT 723;"WF1.1,1,1.2,0T" !DISABLE INTERNAL TRIGGER
1901 OUTPUT 723;"WF1.1,3,1.2,0T" !TRIGGER POLARITY SELECT INPUT DISABLED
1902 OUTPUT 723;"WF1.1,4,1.2,1T" !EXT LOGIC SENSE ACTIVE HIGH
1903 OUTPUT 723;"WF1.1,5,1.2,1,T" !EXTERNAL LOCKOUT-INPUT ENABLED
1904 OUTPUT 723;"WF1.1,7,1.2,0T" !MULTIPLE EXTERNAL TRIGGER RESPONSE
1905 OUTPUT 723;"WF1.1,20,1.2,1T" !PROGRAM GAIN X10(FOR LSR OF .0005)
1908 RETURN
1916 Purge:
1920 FOR I=65 TO 66
1930   Lucky$=CHR$(I)
1940   PURGE Lucky$
1950 NEXT I
1960 FOR I=65 TO 66
1970   Lucky$=CHR$(I)
1980   CREATE B0AT Lucky$,8192,16
1981   ASSIGN @Path2 TO Lucky$
1982 NEXT I
1983 PRINT USING "///"
1985 PRINT "HAD TO PURGE AND CREATE B0AT FILES"
2000 RETURN
3000 END

```

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